

Reviewed NOV 28 1948

An attempt at Ultimate Design.

See p. 106

Requirements:-

- 1: Minimum clearance; and steam-tight joints.
- 2: good Isolation of Inlet-steam; Good Isolation of Crank-Case (vacuum).
- 3: Minimum Radiation, & Conduction Losses, with minimum neat Insulation.
- 4: simple Arrangement, for Cheap Manufacture & Maintenance.
- 5: Low Cylinder-Wall & Piston-Ring Temperature: Jacketed if possible.
- 6: High Expansion-Ratio, (see p. 102). [Study Ajax Marine-Engine]
- 7: Standard Connecting-Rods, & Bearings.
- 8: No Cam-shaft, nor gears. (?? why not??)

Doble Papers
Duple Library

AUG 23 1945

Items	Notes & Calculations for his Steam-Car: Installation of Doble Boiler	Remarks
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A Feed-Pump Capacity & Engine-Consumption:-

- 1: For Doble model F Boiler, what capacity & size of Feed-Pumps?
Use following data furnished by Mr. Keen:-
a: Stanley Engine (10 hp): $3\frac{1}{4}$ Bore x $4\frac{1}{4}$ Stroke, geared 34:41 to $26\frac{1}{2}$ dia Drivers. Assume Engine Inlet-Steam to be 700° F.
b: Car weight = 2,800 lbs; assume 3,000 lbs with driver, etc.

His letter of June 25th 1948
600 psi Boiler Press.
Is $13\frac{1}{4}$ the Rolling Radius
Probably 600 F

c: Grade-Tests:	Miles/Hr.	Steam Chest Press.	Cut-Off (assumed)
$2^{\circ} = 3\frac{1}{2}\%$	45 to 50	250	$\frac{1}{3}$
$5^{\circ} = 8\frac{3}{4}\%$	25	350 to 375	$\frac{1}{3}$
$7^{\circ} = 12\frac{1}{4}\%$	15	350 to 375	$\frac{1}{3}$

2: Total-Resistance: Assuming .015 R.R. & No R_{AIR} & no acceleration for $12\frac{1}{4}\%$ grade = 45 lbs R_R + 367 lbs R_G = 412 lbs total R.

3: On $12\frac{1}{4}\%$ grade, assume leakage through Engine cancels the volumetric-deficiency: i.e., cu. displacement net = 100%.

a: $3\frac{1}{4}$ Bore = 8.296 Sq. in. x $4\frac{1}{4}$ Stroke = 35.28 cu in./stroke, x 4 strokes = 141 cu in. x $\frac{1}{3}$ Cut-Off = 47 cu in. Net / Rev.

b: Steam @ 375 psi & 700° F (sic) = 1.6916 cu. ft. / lb.

c: 15 mi/hr: $13\frac{1}{4}$ R-Rad, or $26\frac{1}{2}$ R-Dia (sic) x $\pi \div 12 = 6.94$ ft/rev & for 5,280 ft (1 mile) = 760 revs/mile x $\frac{41}{24} = 916$ Eng. Revs/mi so, @ 15 mi/hr. Engine speed = ~~229 Rpm~~. Say 229 Rpm.

d: 47 cu in./rev (net) x ~~229~~ $\frac{229}{24} = 9.54$ = 1,178 $\frac{6.228}{24}$ cu in./min $\div 1,728 = 7.22$ cu ft/mi
OR: ~~229~~ $\frac{229}{24}$ cu ft./mile $\div 1.6916$ cu ft/lb = ~~229~~ $\frac{229}{24}$ $\div 1.6916 = 14.74$ lbs/mile
($\div 8.33 = 1.77$ gals/mile (approx.)) x 27.82 cu in/lb = 410 cu in/mile
If 90° feed = .016 cu ft/lb. ~~or .036 lbs/cu. in.~~ or .036 lbs/cu. in.

.0161 cu ft/lb.
= 27.82 cu in/lb.
= .0359 lbs/cu in

4: His present Feed-Pumps $\frac{5}{8}$ dia x 4" stroke & geared from back-axle @ 13168; 760 Axle revs/mi x $\frac{13}{50} = 212\frac{1}{2}$ Rpm

His letter of June 22 1948

Charles F. Keen : Continued Feed-Pump Calculations.

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Remarks.

Items

cont 4: a: Present Pumps make $212\frac{1}{2}$ Revs/mile.

b: $\frac{5}{8}$ " bore = .3068 Sq.in. x 8" Stroke (2 pumps)/rev = 2.45 cu.in. (2.4344 cu.in.)
 $\times 212\frac{1}{2} = 522$ cu.in./mile $\div 27.82$ cu.in./lb = 18.75 lbs/mile
 @ 100% Vol. Eff.; X say .85 = 15.93 net lbs/mile, or Say 16

Doble Papers
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5: On a $12\frac{1}{4}\%$ grade @ 15 mi/hr. Engine requires $14\frac{3}{4}$ lbs/mile. Pumps can deliver @ 85% Vol. Eff. a total of 16 " ", (1.92 gals/mi) thus giving a surplus of $\frac{1}{4}$ lbs/mile. Barely enough. On a heavier grade, with higher Steam-Chest Pressure; or with a lower Steam-Temperature @ Engine; Pumps would be too small, However, they should be OK for present use.

B Diagram of Feed-Water Circuit & Control-Wiring:-

1: Recommend regular Model F Normalizer with Greyhound Control-Box; viz, One pump cuts-in direct from the Pressure-Control (Bus-Bar), & the other (plus Normalizer) cuts-in from Temperature-Control (top-switch, Normally-Open). Made him a diagram of system, and of Control-Box Adjusting-Procedure.

2: a:

C Rebuild of Stanley Engine $3\frac{1}{4} \times 4\frac{1}{4}$

1: Piston-Rod: Assume 500 psi x 8.3 Sq.in. } 4,550 lbs load.
~~Say $\frac{1}{2}$ " dia. = 20 sq.in.~~ Say $\frac{3}{4}$ " dia. = 32 Sq.in. Say $\frac{7}{8} \times \frac{7}{8} = 176$ Sq.in.
 = 5,200 lbs/sq.in.
 300 psi x 8.3 = 2490 Say 3,000 lbs; Say $\frac{3}{4}$ wrist-pin. & say 4,800 psi = .625 Sq.in. = .8.375 Say $\frac{7}{8}$ long.

Say $\frac{9}{16}$ -18 thr'd = .494
 = 1924 Sq.in.
 = 21,600 psi

JAN 11 1949

D: New V Compound for his new Steam-Car!

1: $2\frac{1}{4}$ " H, $4\frac{1}{2}$ " B, x $3\frac{1}{2}$ " Stroke, geared 2:1, = 1,500 Rpm @ 60 mi/hr.
 2: Engine to be bolted to Torque-Tube (no universal-joints), and rubber-suspended between Boiler & Dash, under hood.

MAR 4- 1949

E Conference with Keen re present program:-

1: New Cross-Compound: Same size as in "D" above; but on axle with cylinders at rear like @ on p. 3 (23-1-35) of "Chassis"

JUN 5 - 1949

Feb 7th 1950
 Dropped him
 Poor pay.